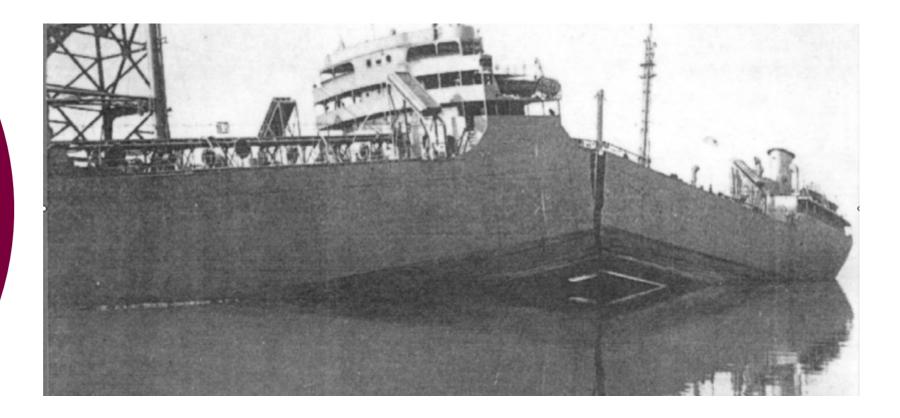
Rebuilding mef90



PETSc June 2023 Blaise Bourdin
https://www.math.mcmaster.ca/bourdin
bourdin@mcmaster.ca
Department of Mathematics & Statistics
McMaster University
Hamilton, ON Canada



Phase-field fracture



Variational Approach to Brittle Fracture

Hypotheses:

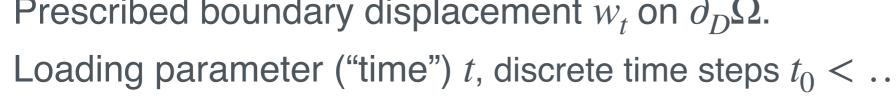
Quasi-static ("rate independent").

Linear brittle/elastic material, domain $\Omega \subset \mathbb{R}^n$.

Hooke's law \mathbf{A} , fracture toughness G_c .

Prescribed boundary displacement w_t on $\partial_D \Omega$.

Loading parameter ("time") t, discrete time steps $t_0 < \ldots < t_N$.



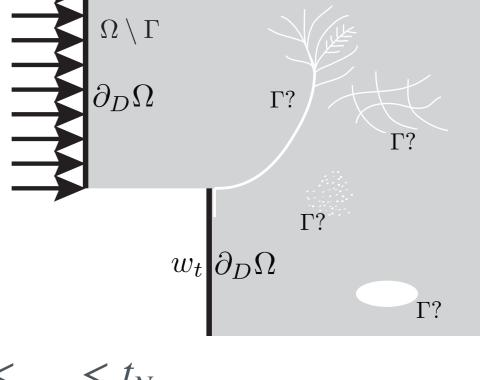
Goal:

Find the equilibrium displacement u and crack geometry Γ without any a priori hypotheses for all $0 \le t \le T$.

Francfort and Marigo Variational model:

$$\mathscr{E}(u,\Gamma) := \int_{\Omega \setminus \Gamma} \frac{1}{2} \mathbf{A} \mathbf{e}(u) \cdot \mathbf{e}(u) \, dx + G_c \mathscr{H}^{n-1}(\Gamma)$$

At each t_i , find (u_i, Γ_i) global minimizers of \mathscr{E} subject to $\Gamma_i \supset \Gamma_{i-1}$.



Numerical Implementation

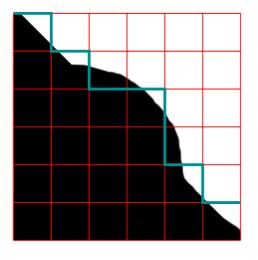
Free discontinuity problem:

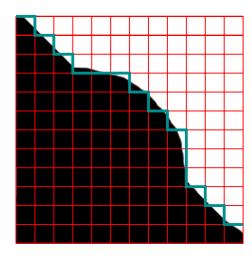
Deal with discontinuous fields along unknown lines / surfaces,

Recover position and length / surface of cracks (mesh independent).

Optimization friendly (do not introduce spurious local minimizers).

Work in 2D and 3D.





Approaches:

Adaptive FE: B-Chambolle '00, Fraternali '07

Discontinuous FE: Giacomini-Ponsiglione '03,'06.

Eigendeformations: Schmidt-Fraternali-Ortiz '07

Level sets: Larsen-Richardson-Sarkis '08, Moës et Al '11,

Allaire-Jouve-Van Goethem '10,

Phase-field: B '98, B-Francfort-Marigo '01, B-Francfort-Marigo '08, ...



Variational phase-field approximation

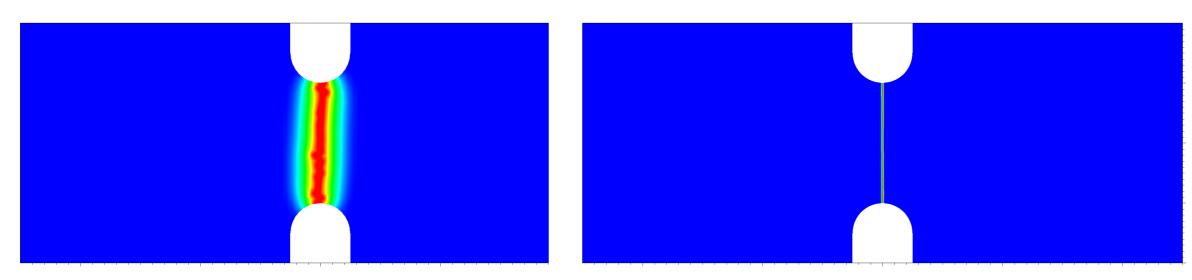
Francfort and Marigo's variational view of Griffith's criterion:

$$\mathcal{E}(u,\Gamma) := \int_{\Omega \setminus \Gamma} W(e(u)) \, dx + G_c \mathcal{H}^{n-1}(\Gamma), \ W(e(u)) := \frac{1}{2} Ae(u) \cdot e(u)$$

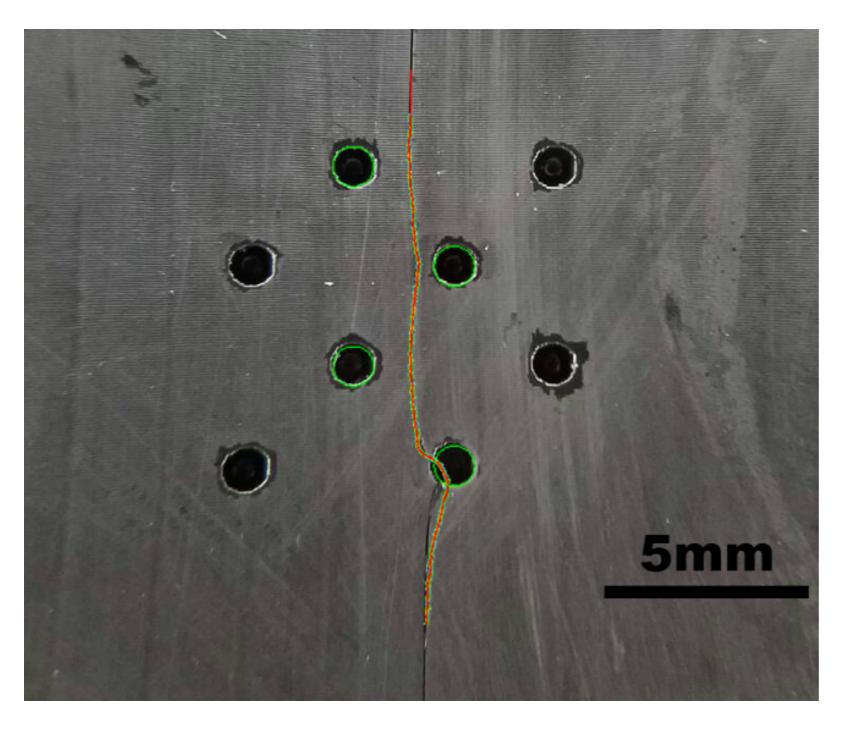
Phase-field approximation (AT₁): $\ell > 0$, $0 \le \alpha \le 1$:

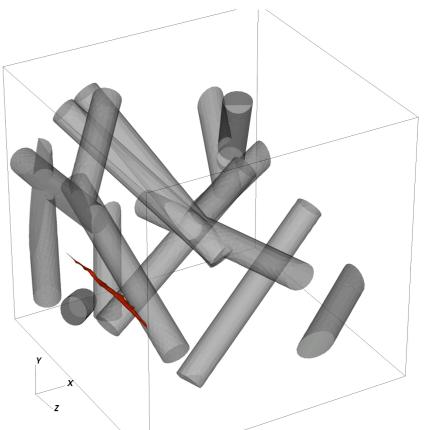
$$\mathcal{E}_{\ell}(u,\alpha) := \int_{\Omega} (1-\alpha)^2 W(\mathbf{e}(u)) \, dx + \frac{3G_c}{8} \int_{\Omega} \frac{\alpha}{\ell} + \ell |\nabla \alpha|^2 \, dx$$

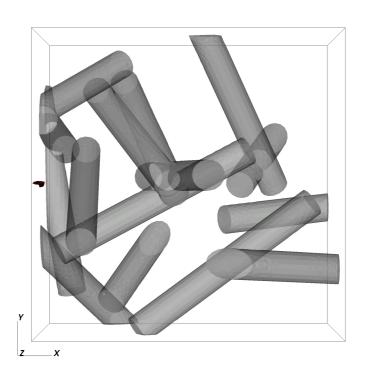
 $\Gamma\text{-convergence of }\mathscr{E}_{\ell}\text{ to }\mathscr{E}\text{ + compactness of }\mathscr{E}_{\ell}\Rightarrow\text{convergence of minimizers}.$



Variational Phase-Field fracture









Fully coupled multi-physics problem

Ductile fracture, fracture + associated plasticity.

$$\inf_{u,p,\Gamma} \int_{\Omega \setminus \Gamma} W\left(\mathbf{e}(u) - p \right) \, dx + G_c \mathcal{H}^{N-1}(\Gamma) + \int_0^T \int_{\Omega \setminus \Gamma} H(\dot{p}) \, dx \, dt$$



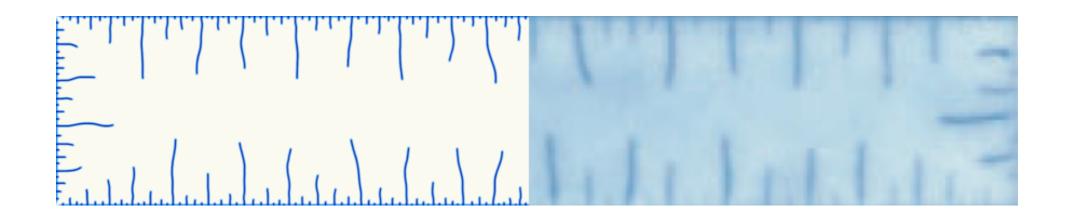


Multi-physics problems: one-way coupling

Thermal cracks, drying cracks.

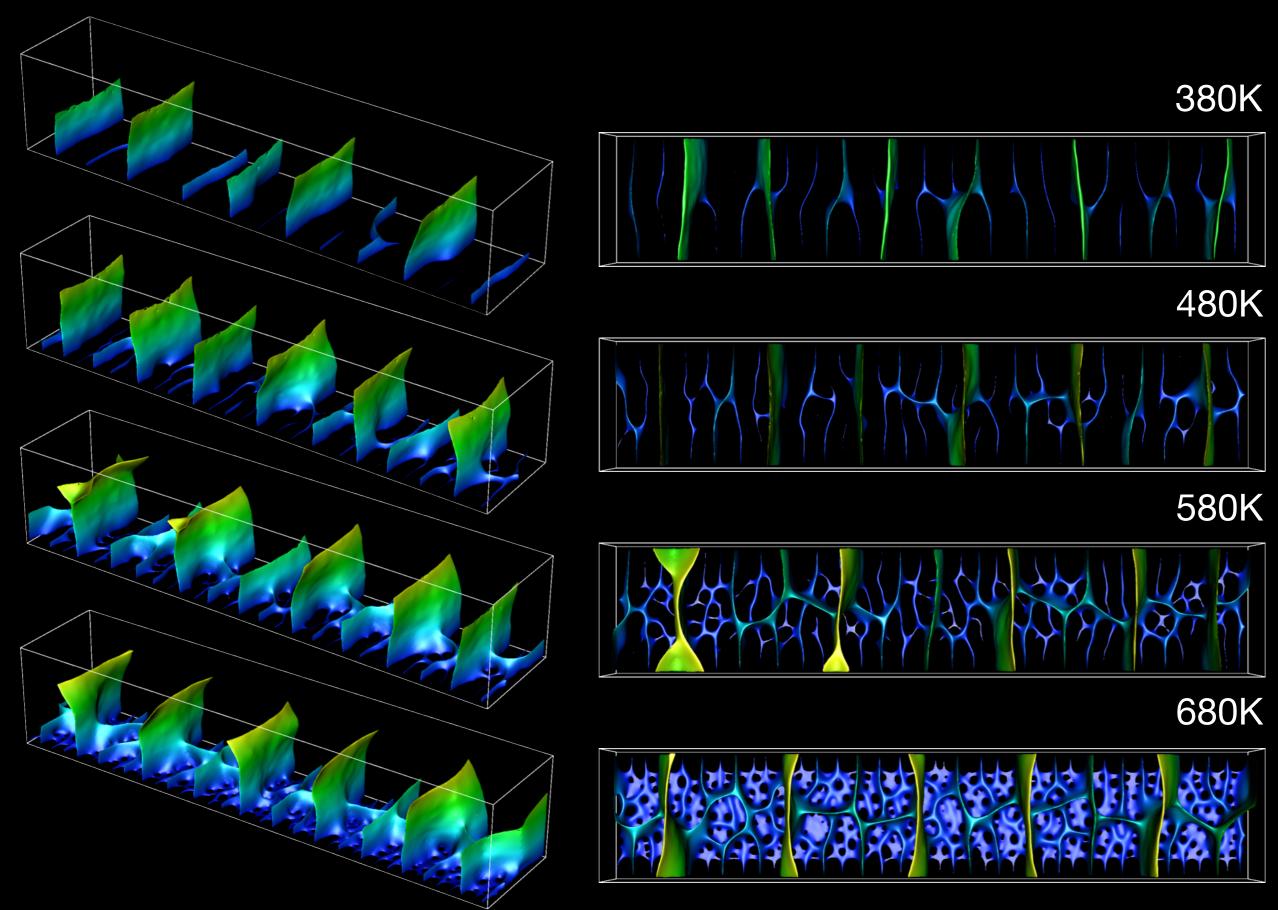
Heat transfer / diffusion on reference (un-cracked) domain).

$$\inf_{u,\Gamma} \int_{\Omega \backslash \Gamma} W\left(\mathbf{e}(u) - \beta T\mathbf{I}\right) \, dx + G_c \mathcal{H}^{N-1}(\Gamma)$$
 subject to $\dot{T} - \nabla \cdot k \, \nabla T = 0 \, \text{in } \Omega$,
$$T(x,0) = \Delta T, \, T(0,t) = 0.$$





2d to 3d transition



Fully coupled multi-physics problem

Hydraulic fracturing.

Mass balance (reservoir part)

Darcy law

$$\frac{1}{M} \frac{\partial p_r}{\partial t} + \alpha \frac{\partial \epsilon_{vol}}{\partial t} + \nabla \cdot \vec{q}_r = q_{rs},$$

$$\vec{q}_r = -\frac{K}{\mu} \left(\nabla p_r - \rho \vec{g} \right).$$

Boundary conditions:

Continuity:

$$\begin{split} p_r &= \bar{p} \text{ on } \partial_D \Omega \text{, } \vec{q}_r \cdot \vec{n} = q_n \text{ on } \partial_N \Omega \\ p_r &= p_{\textit{f}}, \, q_l = - \left[\! \left[\vec{q}_r \right] \! \right] \cdot \vec{n}_\Gamma \text{ on } \Gamma \end{split}$$

Mass balance (crack part)

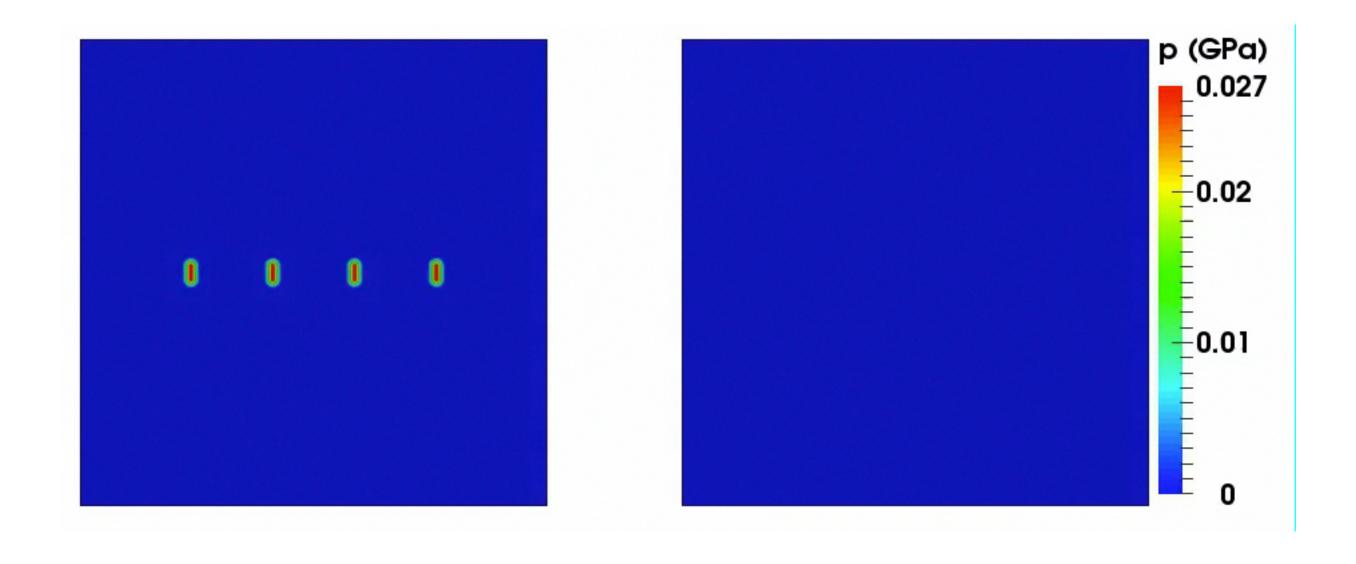
Poiseuille law

$$\frac{\partial w}{\partial t} + \nabla_{\Gamma} \cdot (w \vec{q}_f) + q_l = q_{fs},$$

$$\vec{q}_f = -\frac{w^2}{12\mu} \nabla_{\Gamma} p_f, w = - [u] \cdot \vec{n}_{\Gamma}.$$

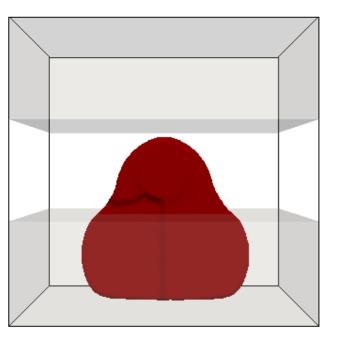


Interacting hydraulic cracks

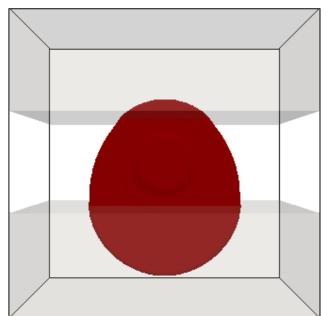




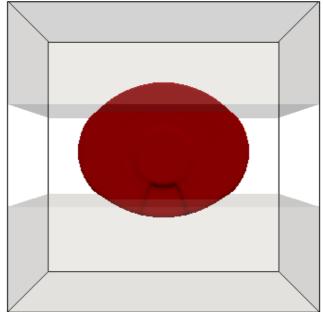
Hydraulic fracturing in layered reservoir



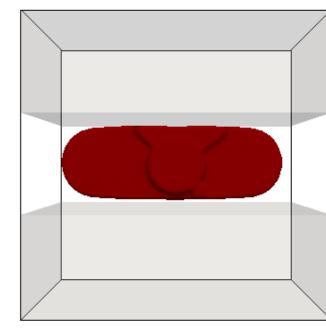




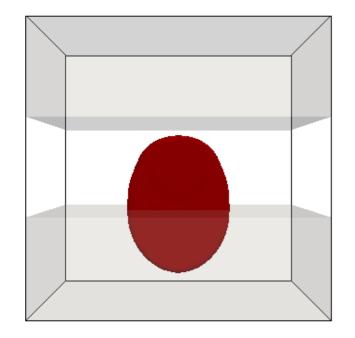
 $G_c^{ext}/G_c^{mid} = .9$



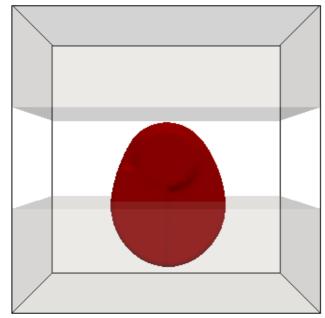
 $G_c^{ext}/G_c^{mid} = 1.2$



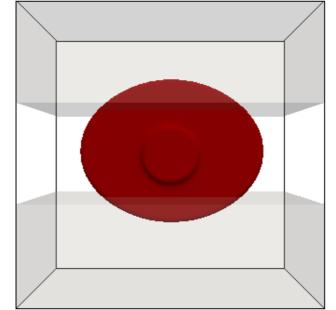
 $G_c^{ext}/G_c^{mid} = 10$



 $k^{ext} = 10^{-15} \text{ m}^2$ $k^{mid} = 10^{-13} \text{ m}^2$

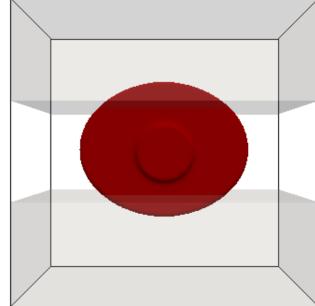


 $k^{ext} = 10^{-15} \text{ m}^2$ $k^{mid} = 6 \cdot 10^{-14} \text{ m}^2$



$$k^{ext} = 8 \cdot 10^{-14} \text{ m}^2$$

 $k^{mid} = 10^{-15} \text{ m}^2$



$$k^{ext} = 10^{-13} \text{ m}^2$$

 $k^{mid} = 10^{-15} \text{ m}^2$



Rate independent processes

General form (discrete in time)

$$(u_i, \alpha_i) = \arg \min_{\alpha_i \ge \alpha_{i-1}, \ \dot{p}_i = G(p_i, u_i, \alpha_i) = 0,} E(t_i, u_i, \alpha_i, p_i)$$

Generalization of quasi-static problems in variational form Solid mechanics (elasticity, plasticity, damage, fracture, ...) Image processing (DIC, restoration, denoting, ...)

R.I.P. vs standard formalism

Time-dependent problems but not ODE (TS)

Constrained optimization but not time-dependent (PetscAdjoint)

PDE / VI-constrained or multi-level optimization (TAO/SNESVI)

Non-convex but usually separately convex energies



mef90 / vDef

Parallel unstructured 2D/3D finite elements.

P1/P2 Lagrange Finite Elements.

Many phase-field variants, plasticity laws, material symmetries, unilateral contact.

Steady state and transient heat transfer (one-way coupling only).

Staggered solver (block Gauss-Seidel)

At each time step t_i : iterate until convergence

Minimization w.r.t u (elastic equilibrium).

Constrained minimization (or variational inequality) w.r.t α .

Solve for the state variable (transient or steady state from t_{i-1} to t_i)

Globally stable, convergence to a critical point of the regularized energy, monotonically decreasing energy. B '07, Burke-Ortner-Süli '10, '13.

Backtracking algorithm (optimality condition in trajectory state).

BSD license since 2014.

https://github.com/bourdin/mef90

docker: bourdin/mef90ubuntumpicho



mef90 timeline

Mid-90's: "Méthode d'Eléments Finis en Fortran 90"

Started as a project to investigate new fortran features (derived types, overloading, dynamic allocation) for image processing, fracture mechanics, optical design. IBM RS6000, DEC alpha, Solaris.

2003, PETSc 2.1:

Switch to Vec, Mat, KSP. Still sequential.

First parallelization using AO, IS. Painful, unmaintainable...

2006: PETSc 2.3:

Rewrite using LocalToGlobalMapping, TAO.

Could never figure out how to handle the L2G for vector-valued elements...

2008-2010: PETSc 3.1-3.3:

Rewrite using Sieve, SNES / SNESVI.

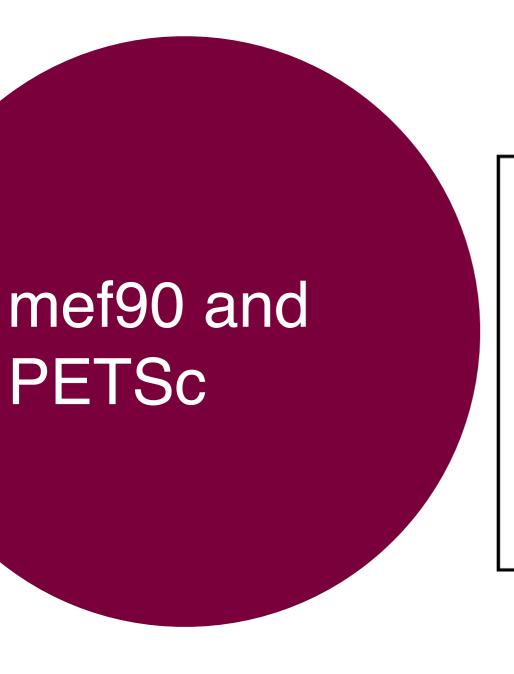
Lots of help from Matt Knepley.

Sieve gets deprecated just as the port is finished...

2022-2023: PETSc 3.17 —

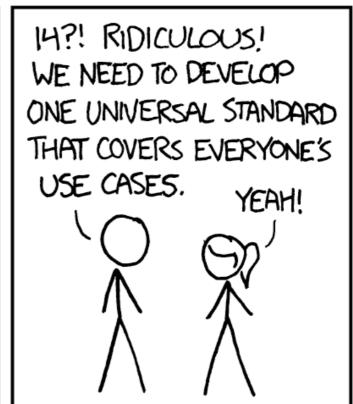
Rewrite using dmplex.





HOW STANDARDS PROLIFERATE: (SEE: A/C CHARGERS, CHARACTER ENCODINGS, INSTANT MESSAGING, ETC.)

SITUATION: THERE ARE 14 COMPETING STANDARDS.



5∞N:

SITUATION: THERE ARE 15 COMPETING STANDARDS.

https://xkcd.com/927/



From sieve to dmplex

Little paradigm changes:

Major simplification to section creation, local assembly routines.

Many creeping "small" changes: dmplex cells must have the same topological dimension, sieve didn't. Locality (or not) of labels.

Main issue was not technical but the lack of documentation of dmplex, PetscSF, PetscSection, PetscLayout.

Fortran bindings, handling of PETSC_NULL objects.

I/O was a pain...



Unstructured mesh I/O

Requirement:

Well-documented, supported binary format. NOT A NEW FORMAT!

Compatibility with modern *and* legacy visualization (TecPlot, ...)

Support for blocks of cells, faces, vertices, "high" order elements.

Strong preference:

Compatibility with mesh generators including industry standard (ABAQUS, hypermesh, MSC-Marc, ...) if possible.

Capable of handling checkpointing and output.

MPI-IO support.

exodusII format.

Limitations:

Cell sets (element blocks) are non-overlapping, consists of sequentially numbered cells. Edge sets are #\$%^*&^%

Standard only *partially* implemented in Vislt, Paraview, meshio, cubit,...



exodusII I/O in natural ordering Why?

Multiple physics / materials in cell blocks, must be made available to visualization / post processing.

"Serialized" distributed dm may not be compatible with exodusII.

vDef wants to be a good citizen and be part of an analysis chain.

"Layouts" of a Vec:

local: Petsc local vector with constraints (non-collective)

global: Petsc global vector without constraints (collective)

cglobal: Petsc global vector with constraints (collective)

natural: cglobal reordered in the initial DM ordering (collective, all values on processor 0 due to limitations of the exodusII format and reader).

IO: natural load-balanced for MPI-IO (collective)

IO2local/local2IO,... PetscSF obtained by composition.





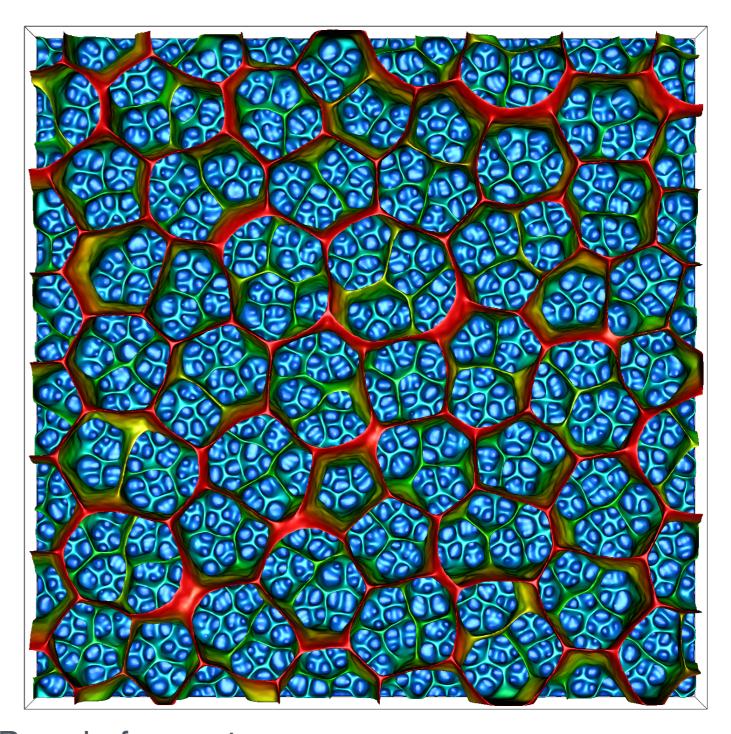
THIS IS GIT. IT TRACKS COLLABORATIVE WORK ON PROJECTS THROUGH A BEAUTIFUL DISTRIBUTED GRAPH THEORY TREE MODEL. COOL. HOU DO WE USE IT? NO IDEA. JUST MEMORIZE THESE SHELL COMMANDS AND TYPE THEM TO SYNC UP. IF YOU GET ERRORS, SAVE YOUR WORK ELSEWHERE, DELETE THE PROJECT, AND DOUNLOAD A FRESH COPY.

Thoughts

- Is PETSc developed for end-users or framework developers?
- Other valuable parts of the PETSc eco-system: test system, makefile system
- Should there be a mechanism to indicate that a PETSc object is still evolving / will become obsolete?
- How to leverage the PETSc community for low-level labour intensive work (documentation, tests, bindings / interfaces)?
- How to incite users to contribute code to PETSc?
 - Have students contribute code early.
 - Contributing to PETSc is a fantastic educational tool.
 - Use PETSc code as reading material.
 - Contributing to PETSc leads to writing better code.







U.S. NSF, LA Board of regents AGC, Corning, Chevron NSERC / CRSNG Canada Research Chair program

